

mid Moulding
Innovation
Day 2025

Metal Injection Molding with Hot Runner Systems: A Direct Injection Approach

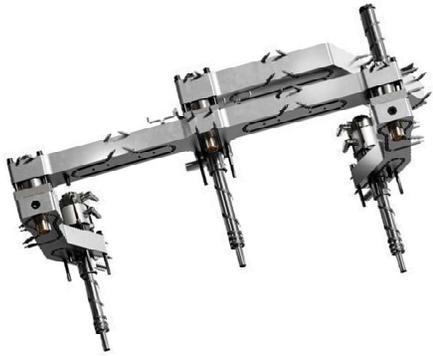
Oerlikon HRS
Luisa Barbisan

Moldex3D



Metal Injection Molding with Hot Runner Systems: A Direct Injection Approach

Division Flow Control - Oerlikon HRSflow



Division Flow Control Oerlikon HRSflow

Polymer Processing Solutions Division

A key enabler for a sustainable polymer processing industry with a focus on manmade fiber plant engineering and flow control equipment solutions.

oerlikon



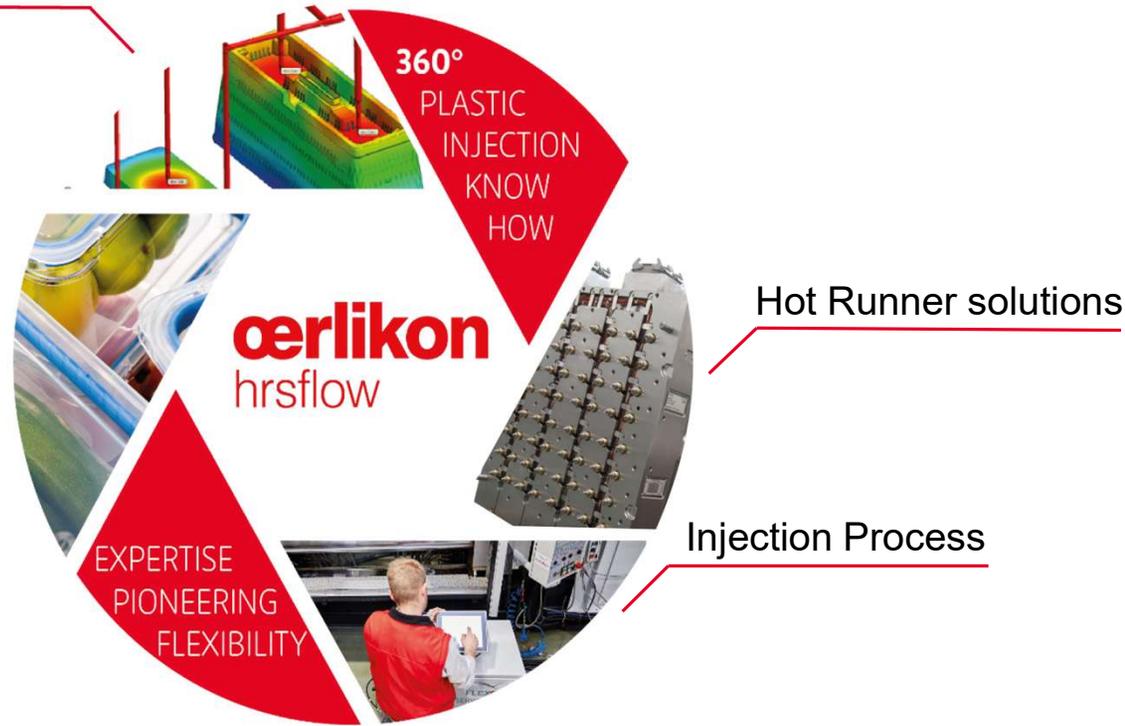
Division Flow Control - Oerlikon HRSflow

Oerlikon HRSflow Know How

360°
PLASTIC INJECTION
KNOW HOW

CAE Simulations

Applications experience

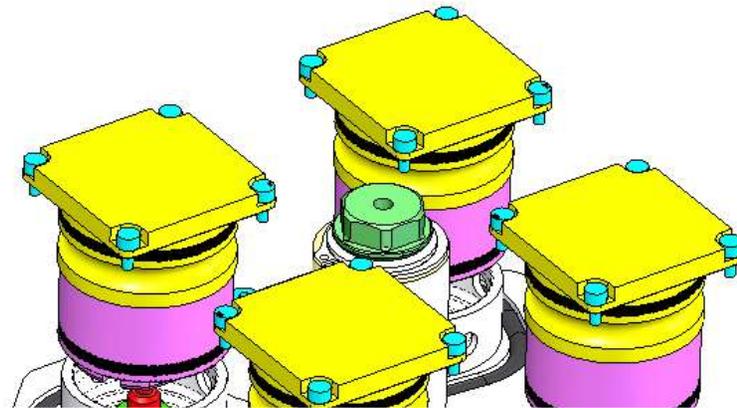


Division Flow Control - Oerlikon HRSflow

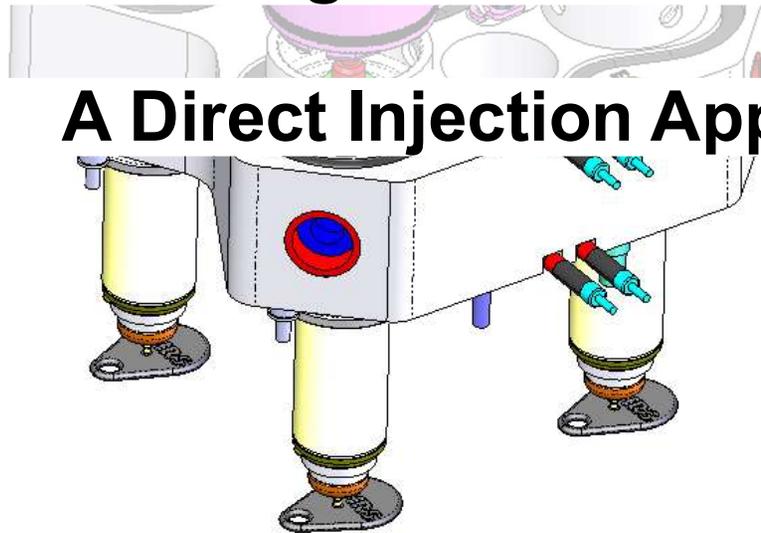
Our Worldwide presence



- 3 production plants (Europe, America, Asia)
- 1035 employees worldwide
- 52 branches worldwide
- 5 CAE calculation pools



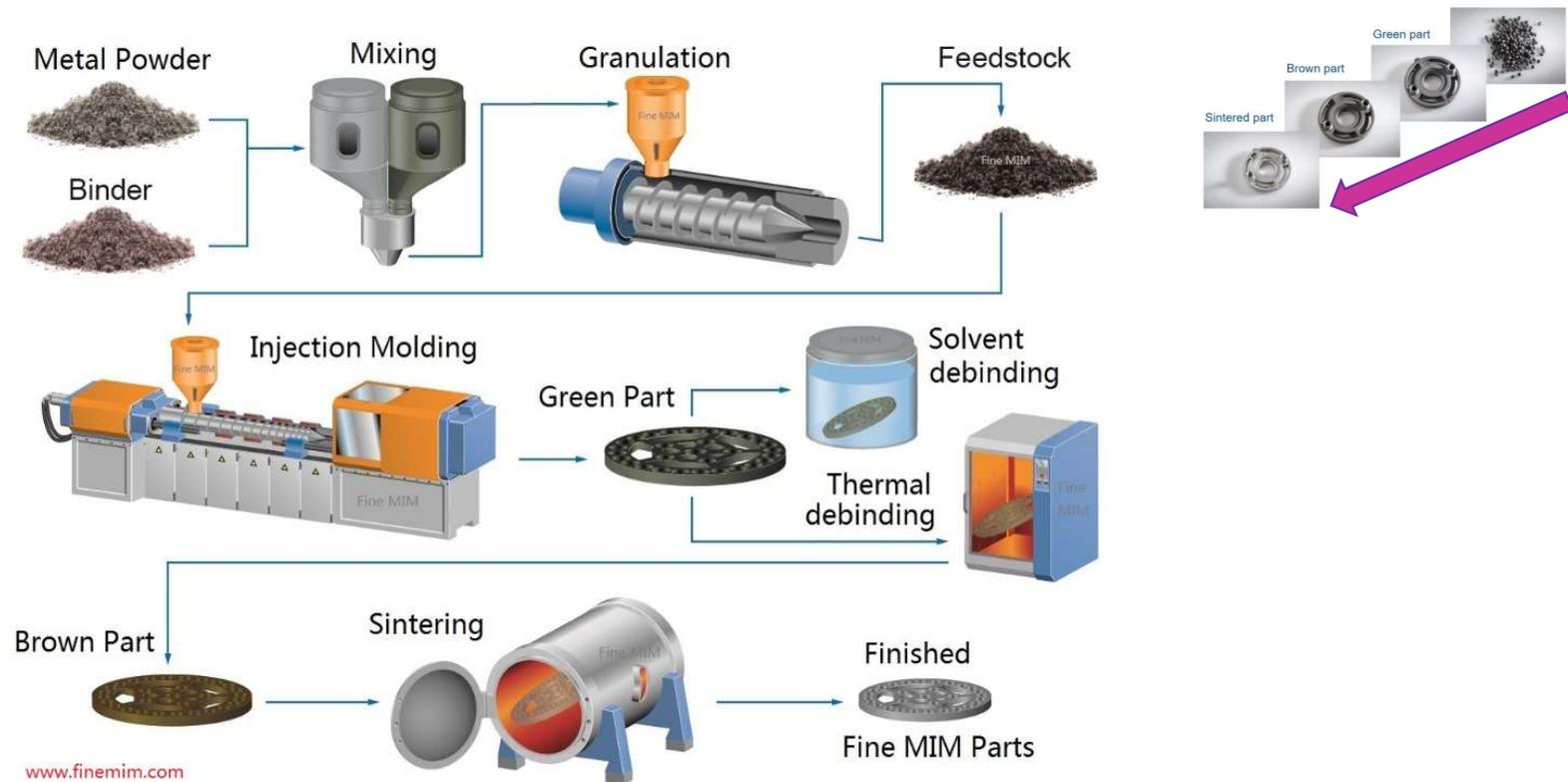
Metal Injection Molding with Hot Runner Systems:



A Direct Injection Approach

Metal Injection Molding

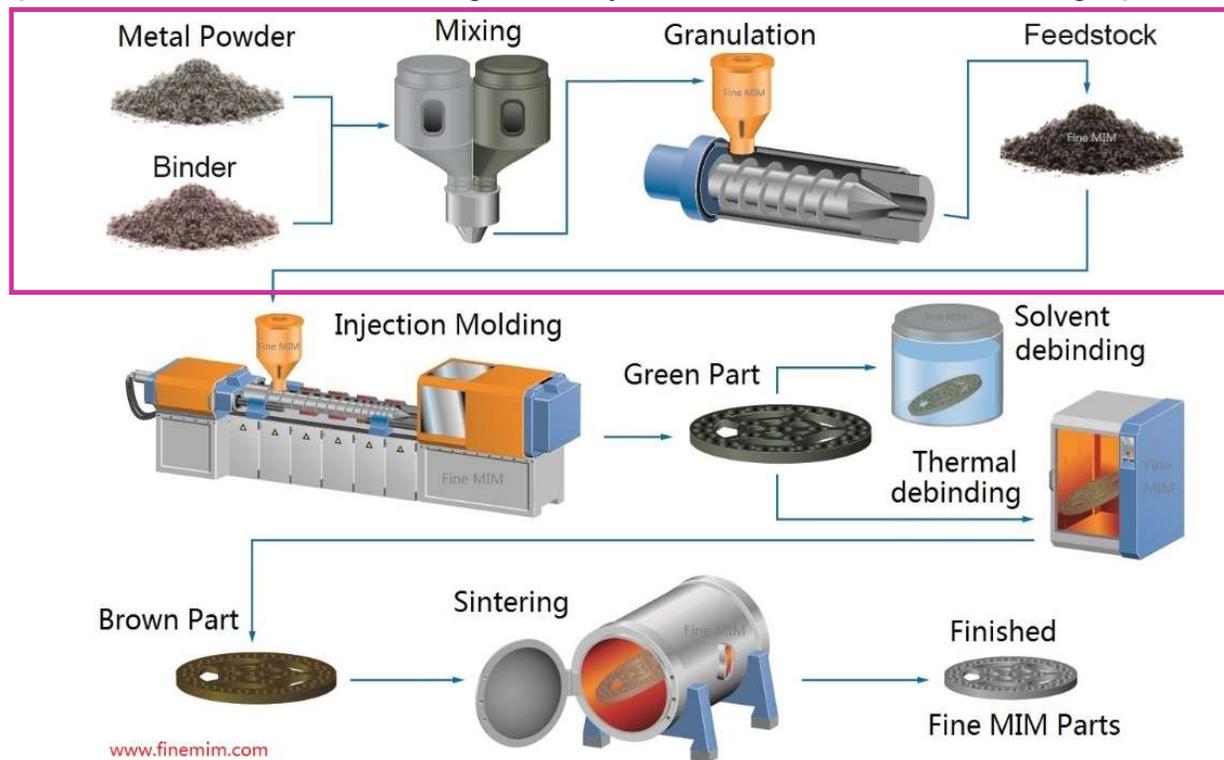
MIM is a process that merges two established technologies: plastic injection molding and powdered metallurgy. It offers a manufacturing capability of producing precise and complex part.



Metal Injection Molding Process

Step 1 - Feedstock: Very fine metal powders are combined with thermoplastic and wax binders in a precise recipe. A proprietary compounding process creates a homogenous pelletized feedstock that can be injection molded just like plastic. This achieves ultra-high density and close tolerances over high-production runs.

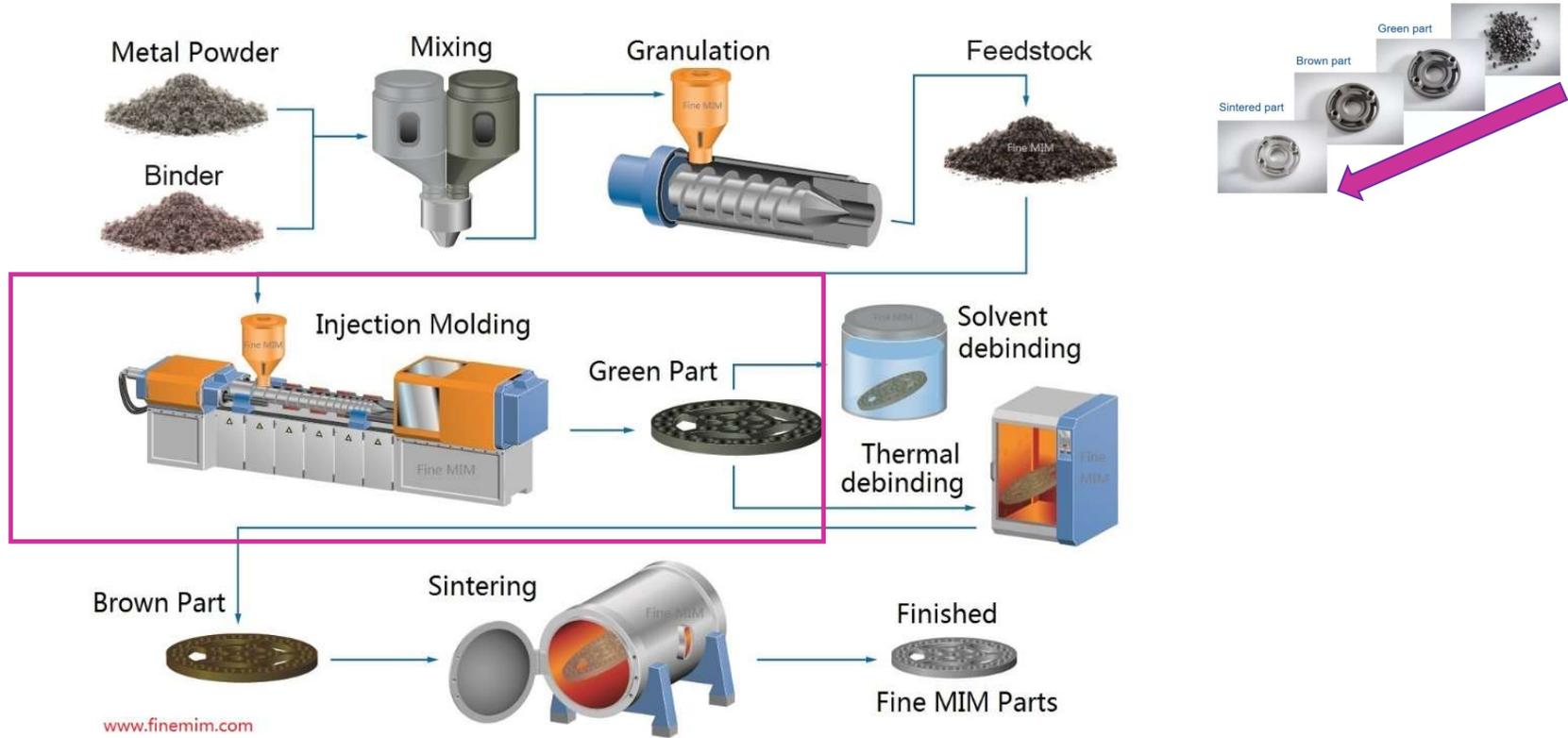
1



Metal Injection Molding Process

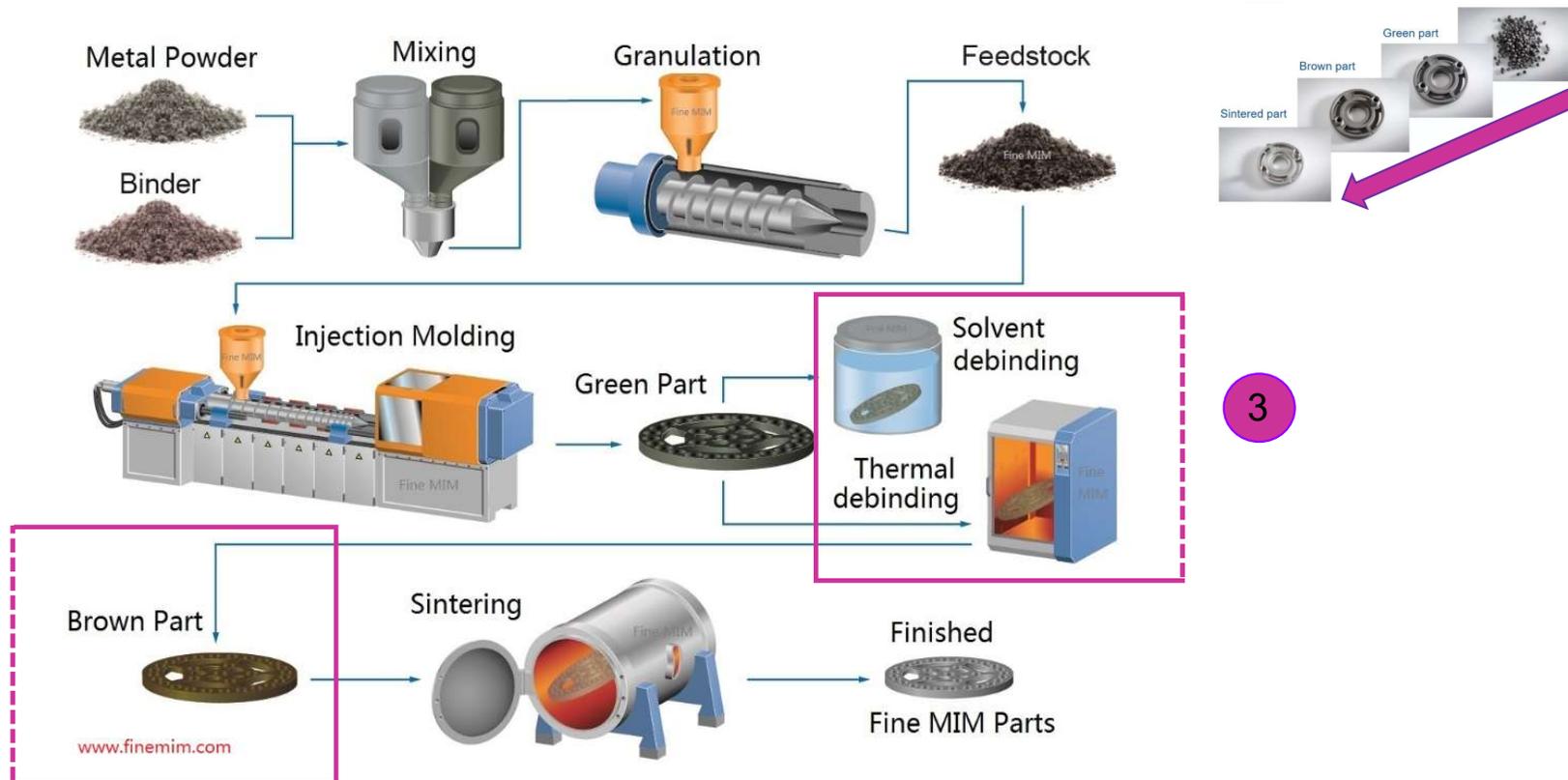
Step 2 – Injection Molding: The feedstock is heated and injected into a mold cavity under high pressure, allowing for extremely complex shapes. Once the component is removed it is known as a "green part."

2



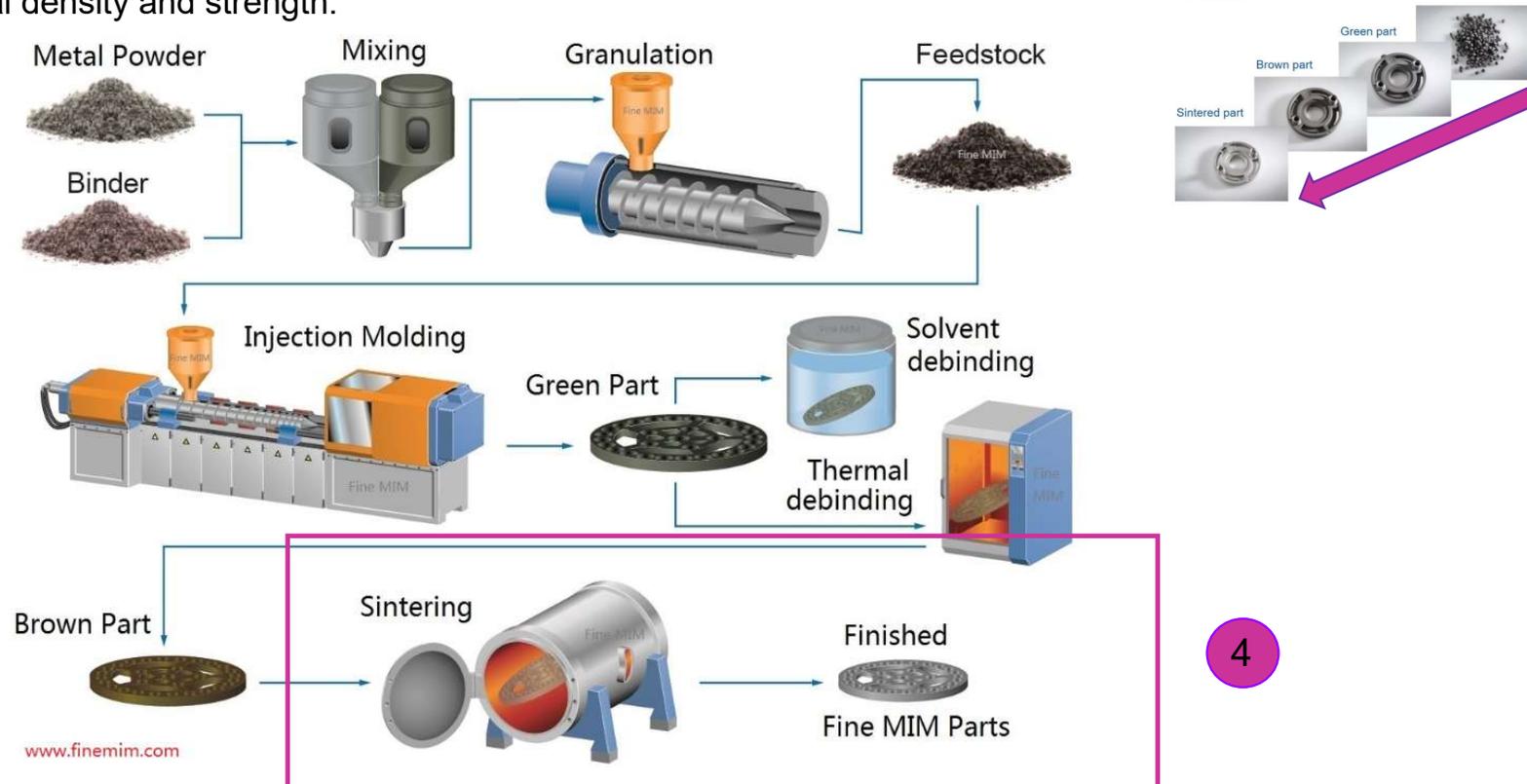
Metal Injection Molding Process

Step 3 - Debinding: the “green part” is then put through a controlled process called debinding that removes the binder and prepares the part for the final step. Once the debinding is complete, the component is referred to as “brown.”

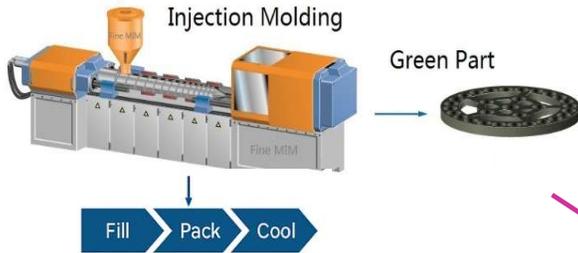


Metal Injection Molding Process

Step 4 – Sintering: the “brown” part is held together by a small amount of binder and is still fragile. During sintering temperatures reach near the melting point of the material. Sintering eliminates the remaining binder and gives the part its final density and strength.



Metal Injection Molding with Moldex 3D

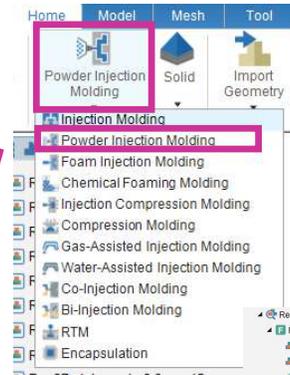


Powder Injection Molding process **Fill + Pack**

Powder Injection Molding module

Material Characterization with **Powder Information**

Total Powder Concentration result: potential surface defect can be predicted in MIM part.



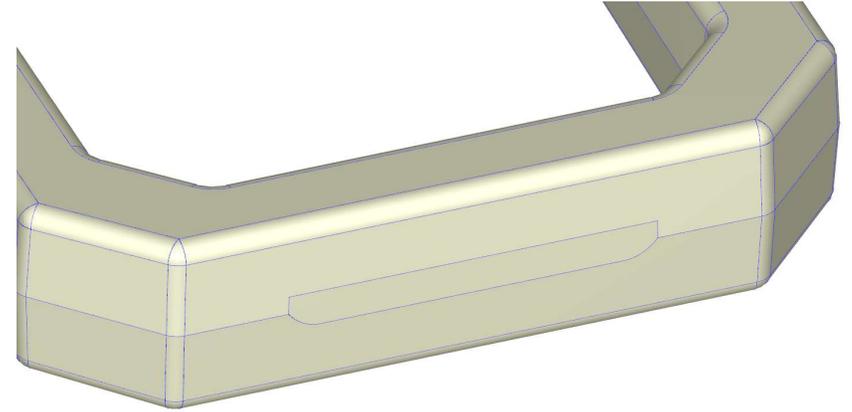
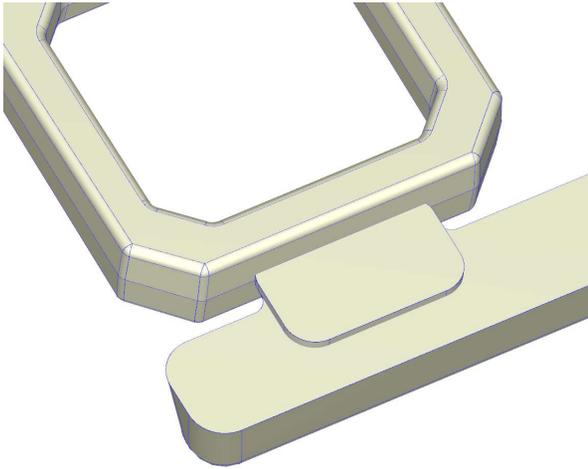
Result F	Value
Filling Time = 0.577 sec (EOF)	0.577 sec (EOF)
Melt Front Time	0.092 sec
Air Zone Volume	0.110 sec
Air Trap	0.138 sec
Weld Line	0.165 sec
Weld Line Meeting Angle	0.191 sec
Weld Line Temperature	0.217 sec
Clamping Force Centroid	0.247 sec
Gate Contribution	0.273 sec
Pressure	0.301 sec
Temperature	0.327 sec
Melt Front Temperature	0.355 sec
Shear Stress	0.380 sec
Peak Shear Stress	0.410 sec
Shear Rate	0.439 sec
Peak Shear Rate	0.463 sec
Viscosity	0.490 sec
Velocity	0.516 sec
Velocity Vector	0.546 sec
Volumetric Shrinkage	0.570 sec (VP Switch)
Density	0.577 sec (EOF)
Welding Angle	
Molten Core	
Frozen Layer Ratio	
Max. Temperature	
Center Temperature	
Average Temperature	
Bulk Temperature	
Max. Volume Shrinkage	
Average Volumetric Shrinkage	
Average Velocity Vector	
Powder Concentration	
Total Powder Concentration	
XY Curve	

Type	PIM
Grade Name	MIM-002
Producer	BASF
Powder Specific	Alloy
Powder Diameter	0.01 (mm)
Average Concentration	60 (vol%)
Powder Density	7.9 (g/cc)

Type	PIM
Grade Name	MIM-002
Producer	BASF
Density	7.9 g/cc
Melt Temperature (Minimum)	180 °C
Melt Temperature (Normal)	190 °C
Melt Temperature (Maximum)	200 °C
Mold Temperature (Minimum)	120 °C
Mold Temperature (Normal)	128 °C
Mold Temperature (Maximum)	130 °C
Ejection Temperature	135 °C
Freeze Temperature	155 °C

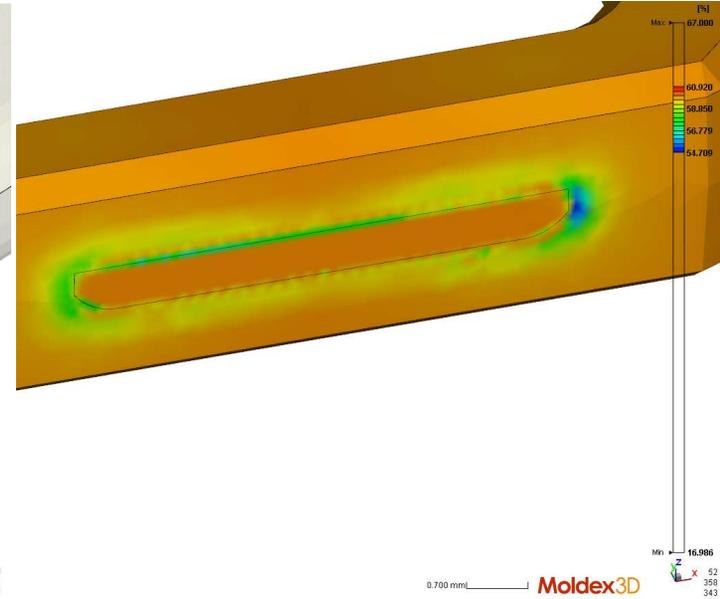
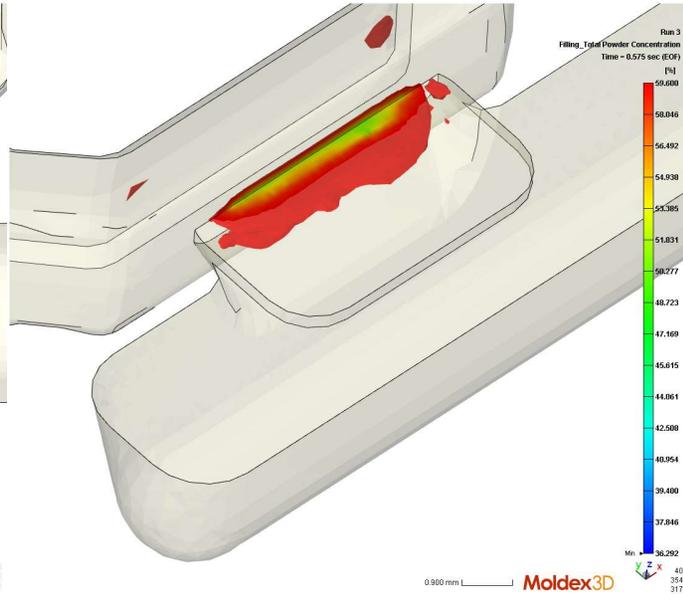
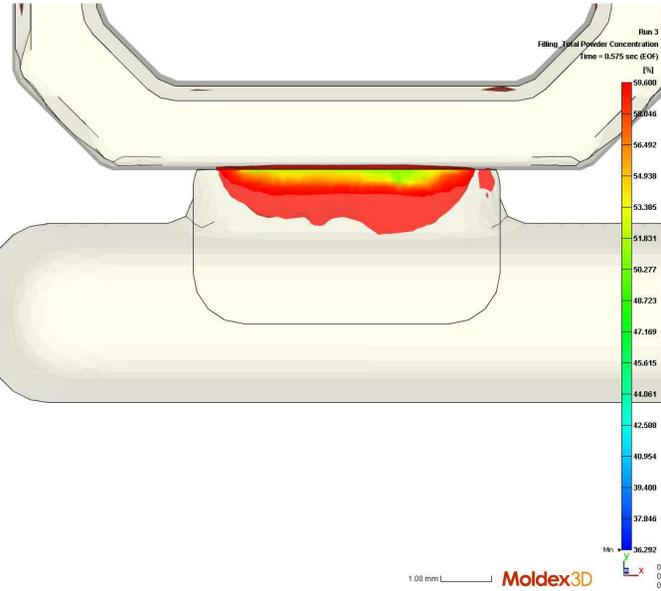
Cold Gate Issue

A cold gate defect prompted an investigation into powder concentration



Powder Concentration Analysis

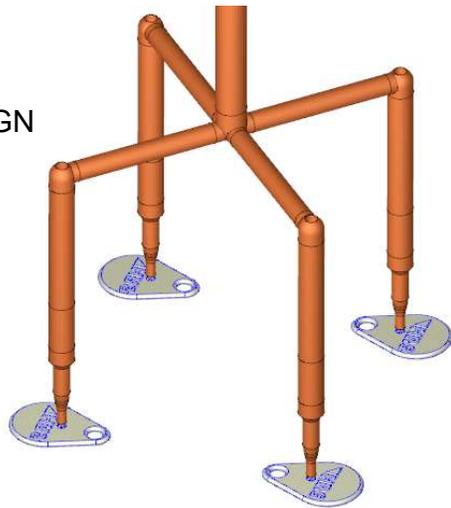
Simulations revealed a black-line phenomenon at the gate area, consistent with what was observed on the molded green part. This issue is linked to powder-binder separation, leading to regions of low powder concentration.



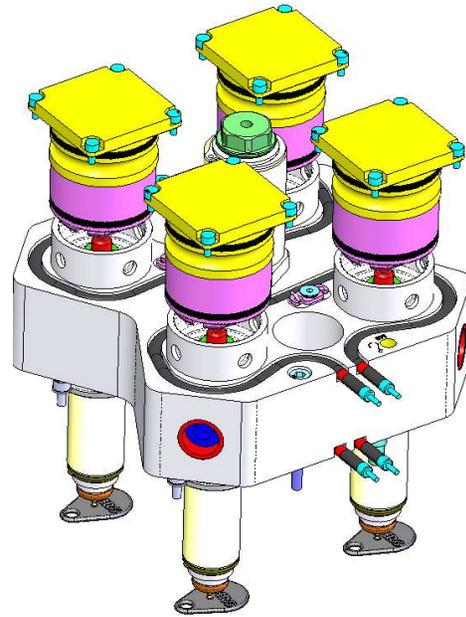
Case Study for Direct Hot Runner Injection



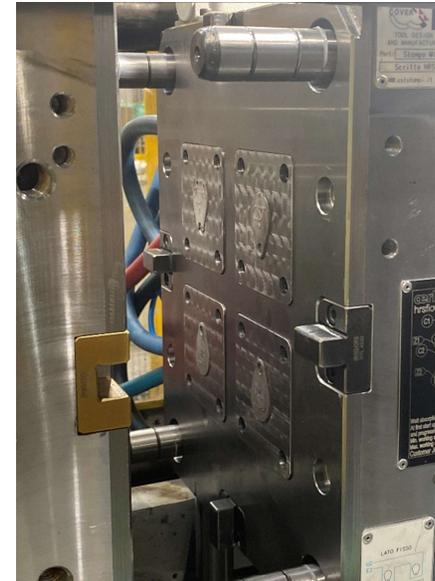
PART DESIGN



MOLDEX 3D SIMULATION



HOT RUNNER SYSTEM PROJECT



TOOL



GREEN PART

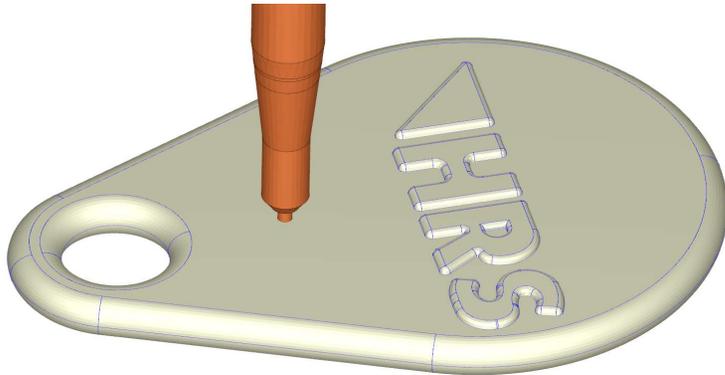


FINISHED PART



Total Powder Concentration on Gate Area

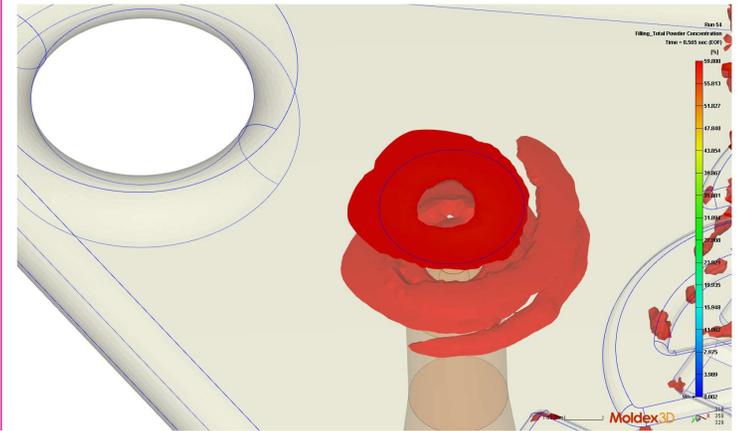
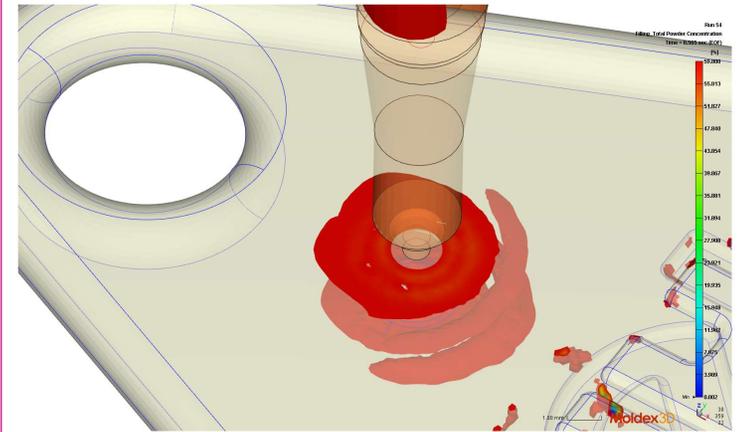
Hot Runner Direct Injection on side A



Side A

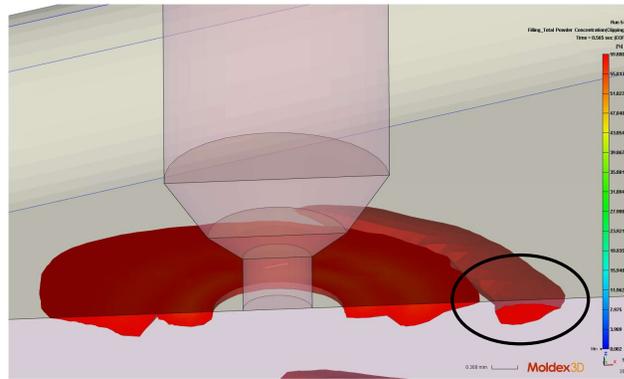


Side B



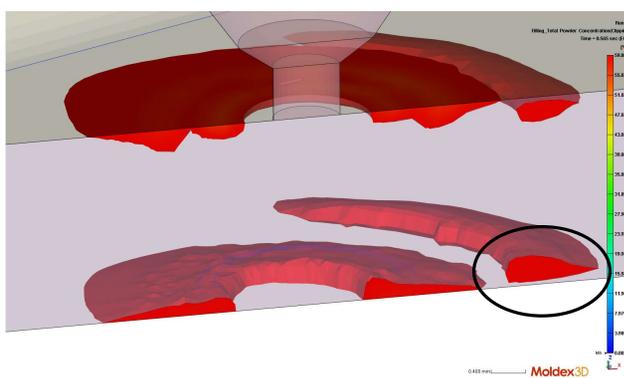
Total Powder Concentration on Gate Area

Side A



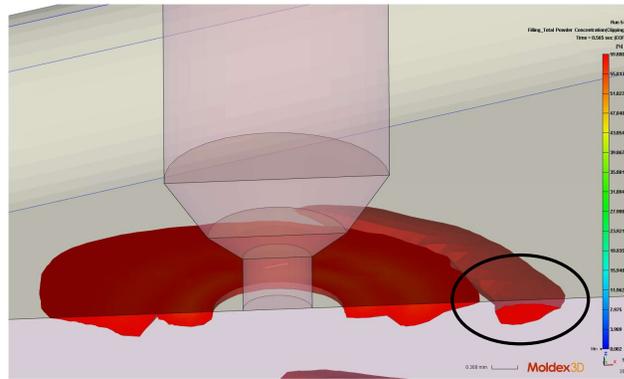
Half-moon marks of lower powder concentration has been noticed under the part skin on both sides.

Side B



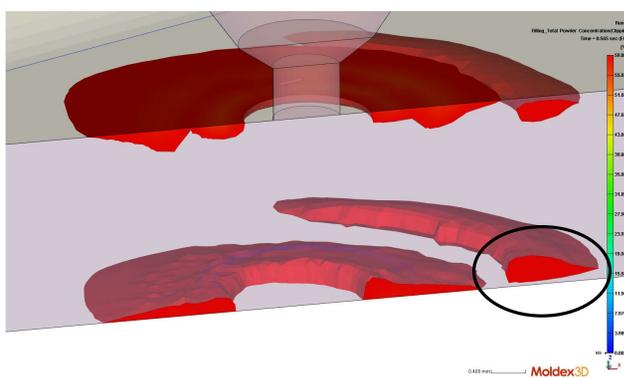
Total Powder Concentration on Gate Area

Side A

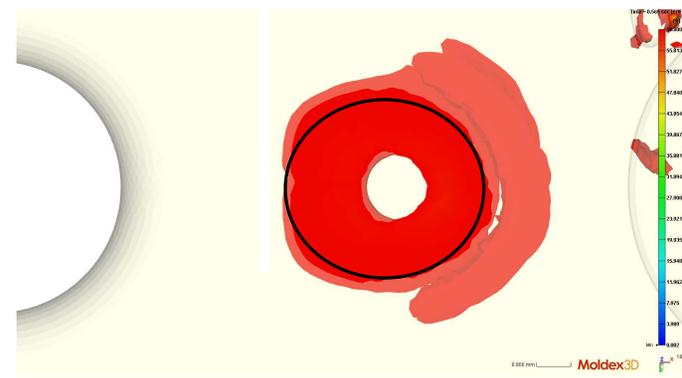


Half-moon marks of lower powder concentration has been noticed under the part skin on both sides.

Side B

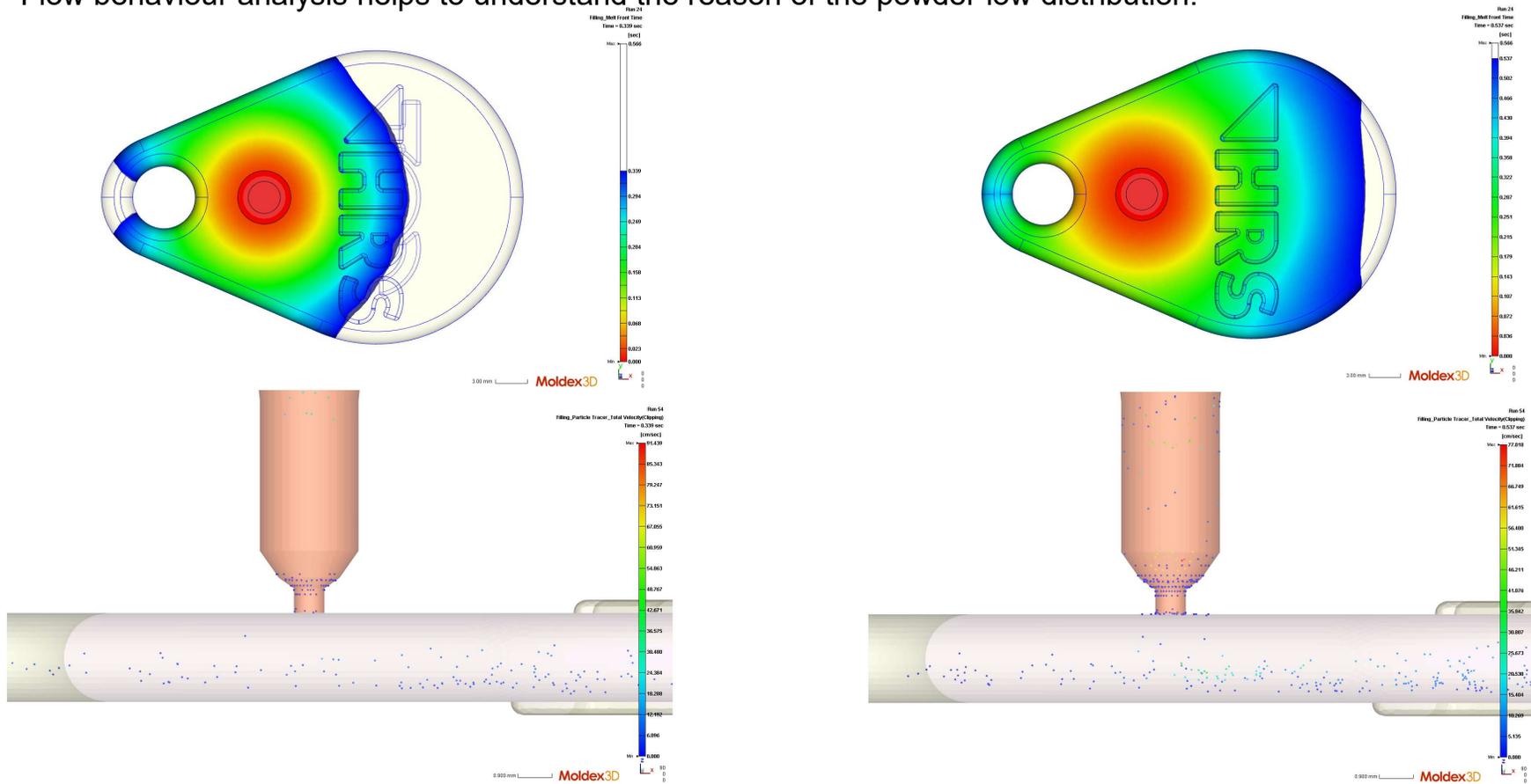


A halo with a lower powder concentration was identified surrounding the injection area on both sides.



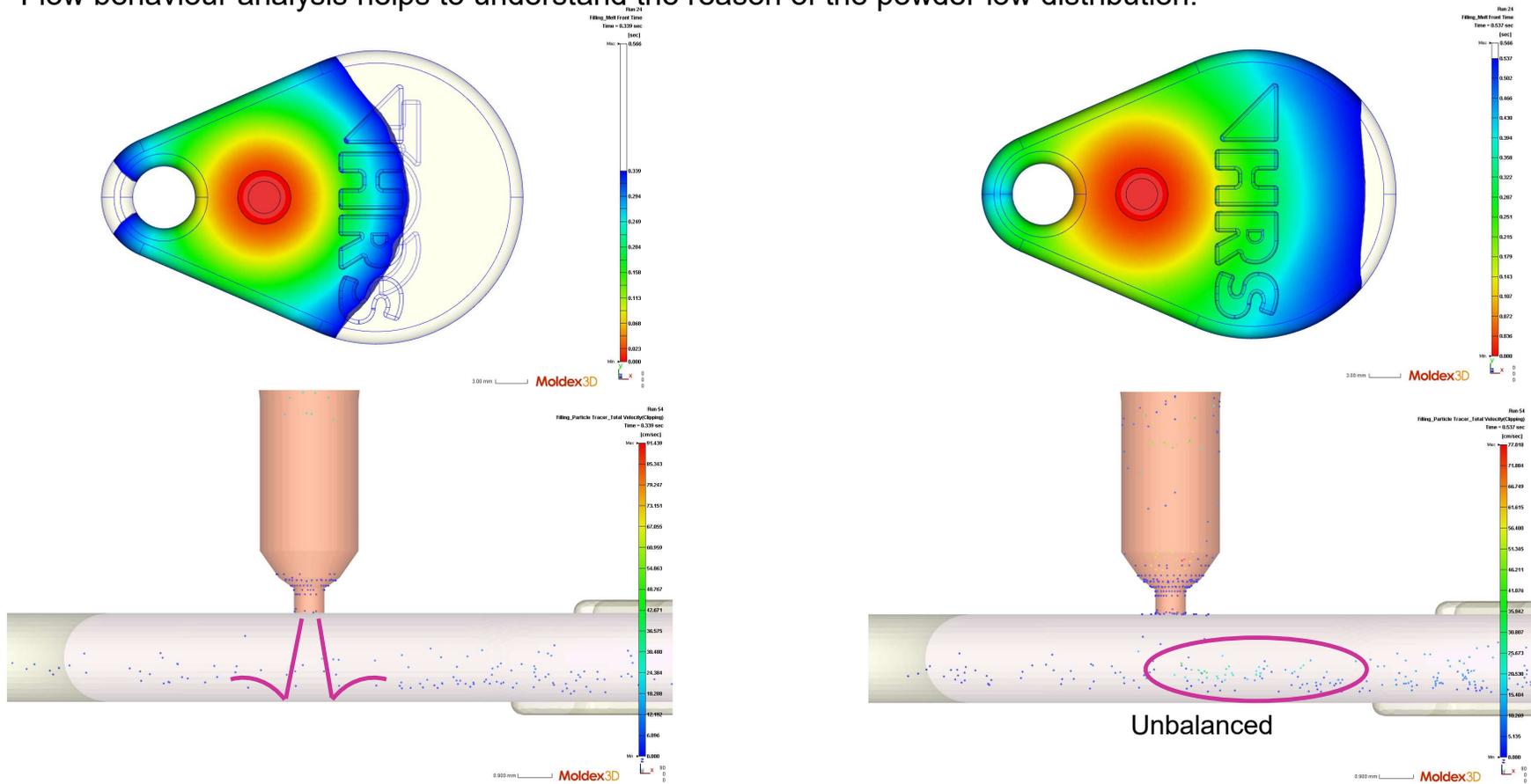
Direct Injection Flow Behaviour at the Hot Runner Gate

Flow behaviour analysis helps to understand the reason of the powder low distribution.

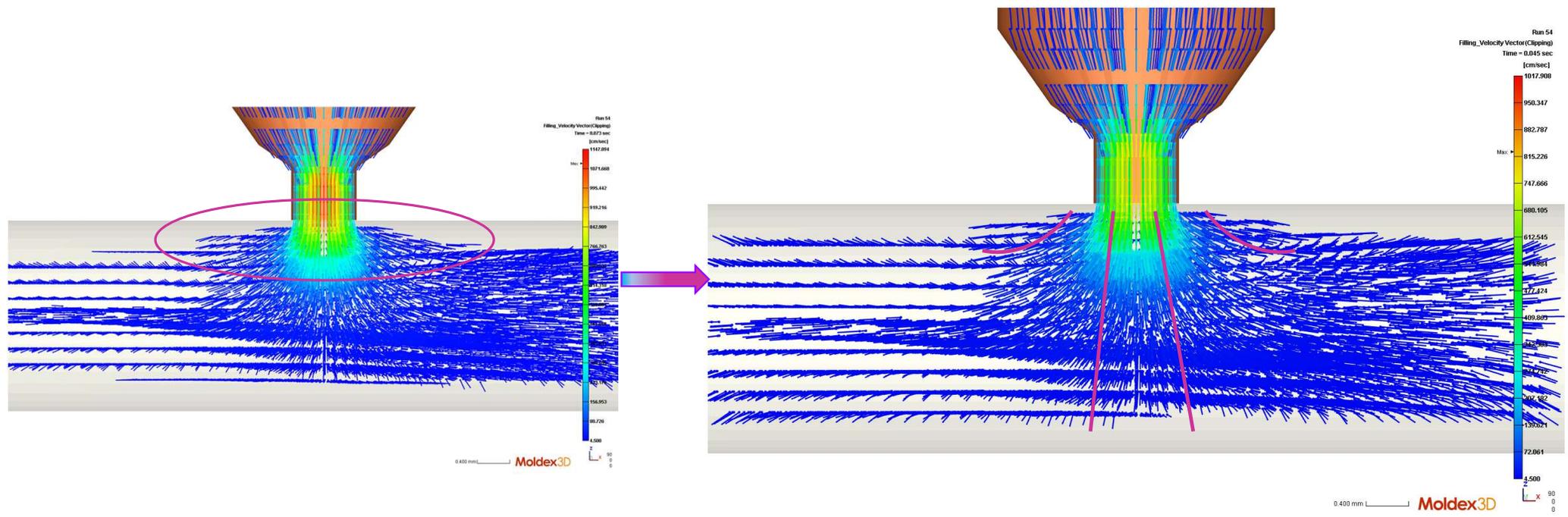


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Direct Injection Flow Behaviour at the Hot Runner Gate

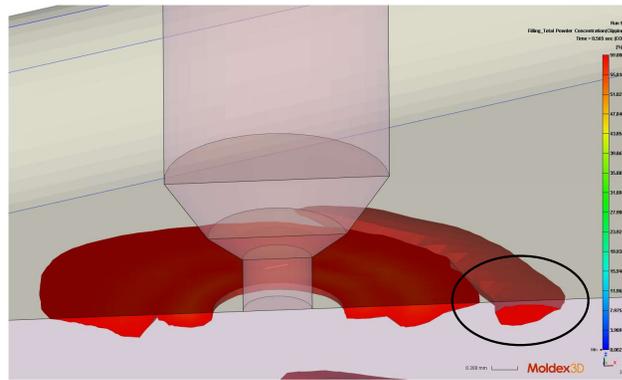


Direct Injection Surface Optimization

Side A



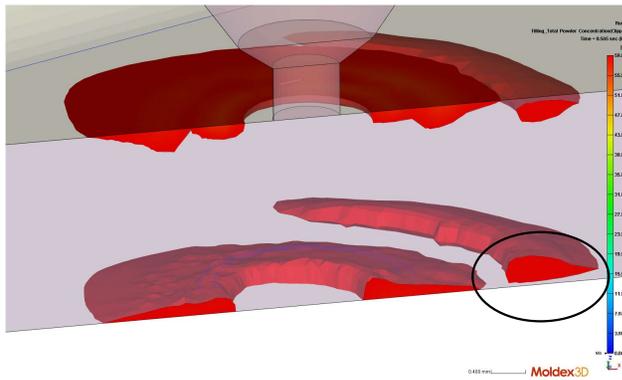
DEFECT



CAUSE

SOLUTION

Side B

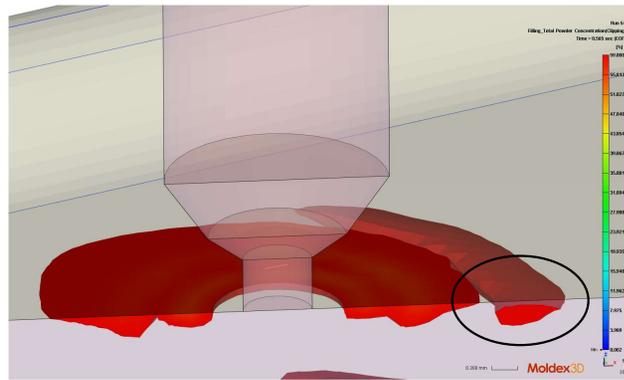


Direct Injection Surface Optimization

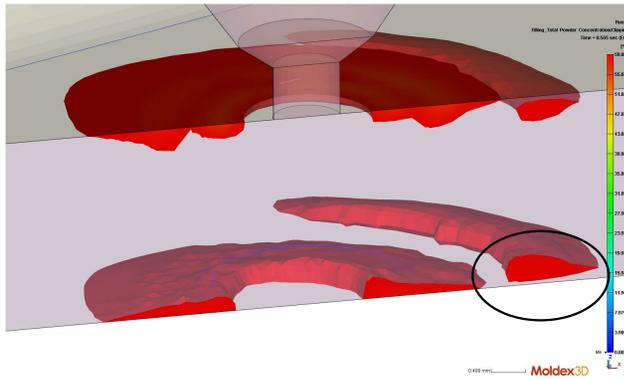
Side A



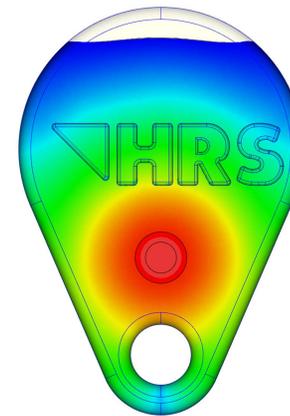
DEFECT



Side B



CAUSE



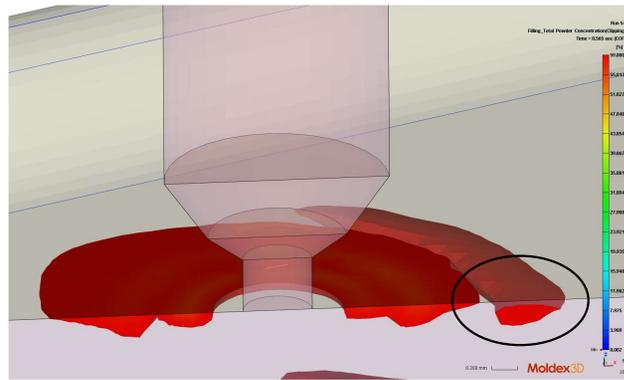
SOLUTION

Direct Injection Surface Optimization

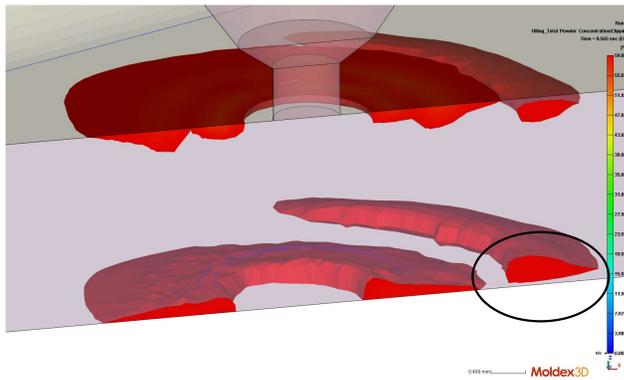
Side A



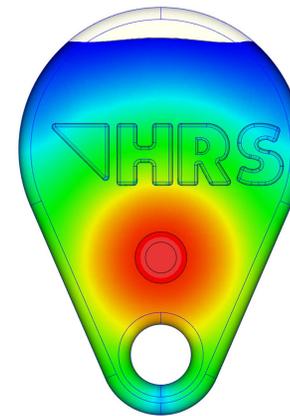
DEFECT



Side B



CAUSE



SOLUTION



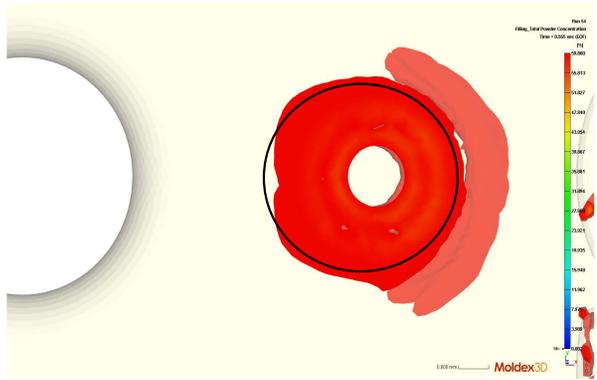
Direct Injection Surface Optimization

SOLUTION

Side A

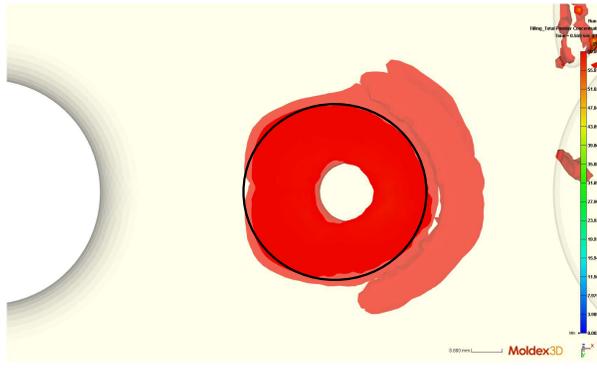


DEFECT



CAUSE

Side B



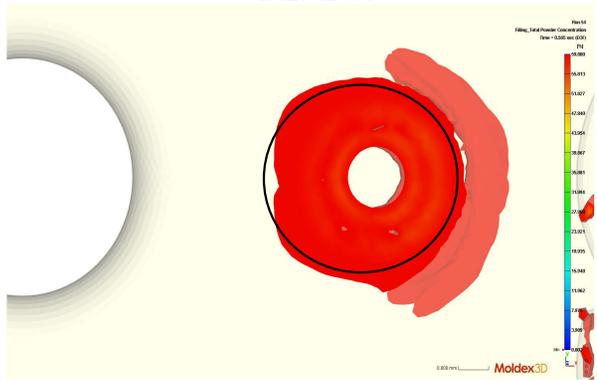
Direct Injection Surface Optimization

SOLUTION

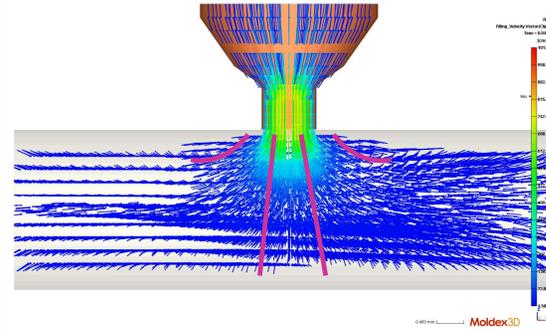
Side A



DEFECT



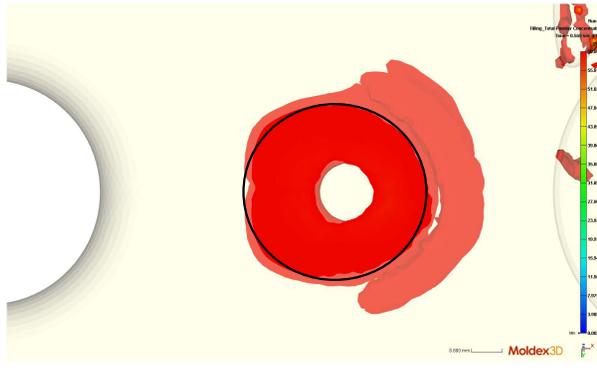
CAUSE



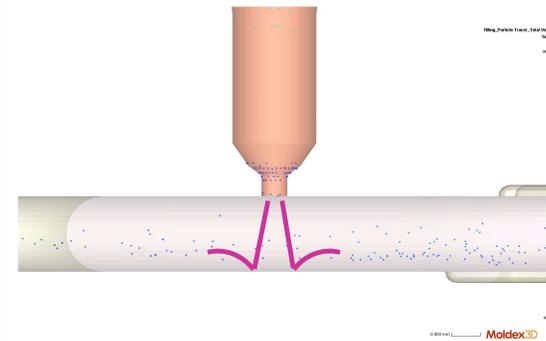
Side B



DEFECT



CAUSE

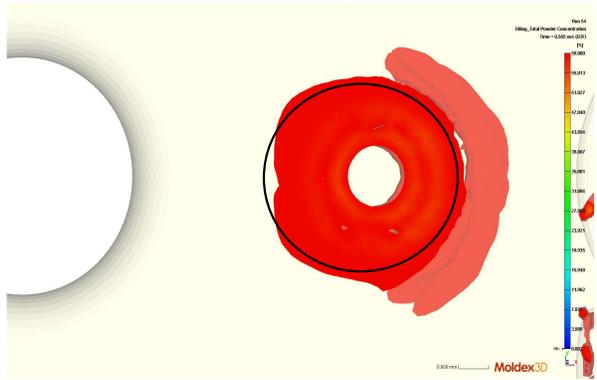


Direct Injection Surface Optimization

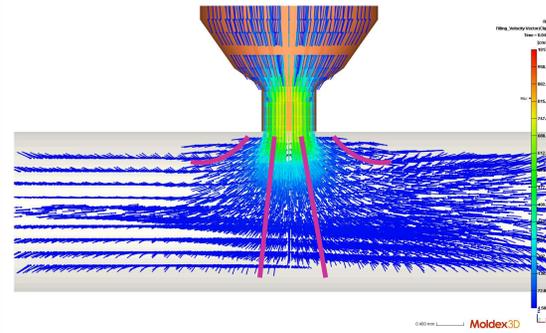
Side A



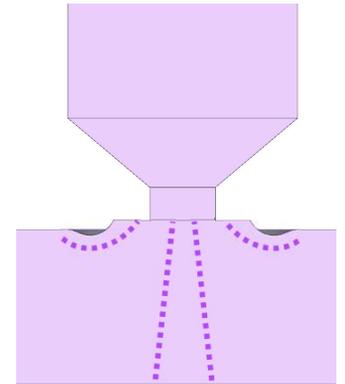
DEFECT



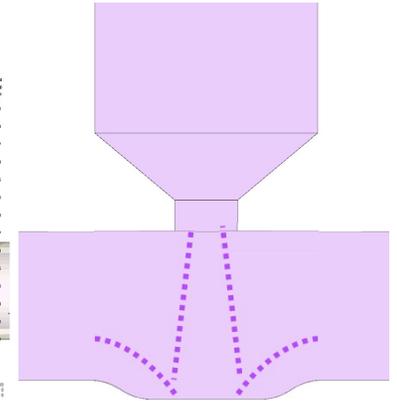
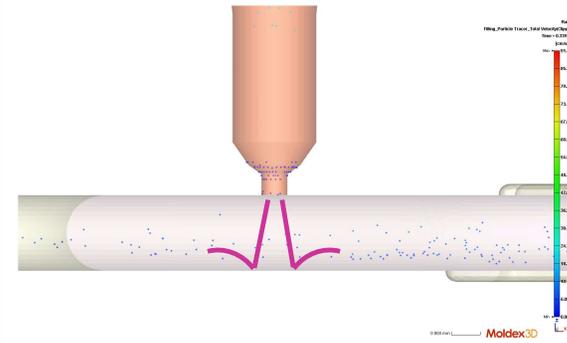
CAUSE



SOLUTION



Side B



Effect of Optimization: Simulation Results

OPTIMIZED DESIGN

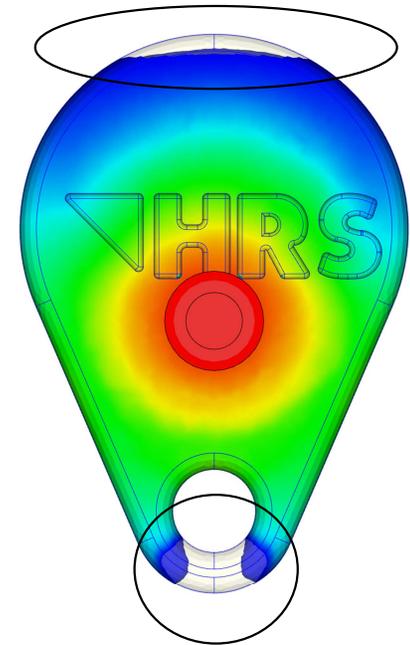
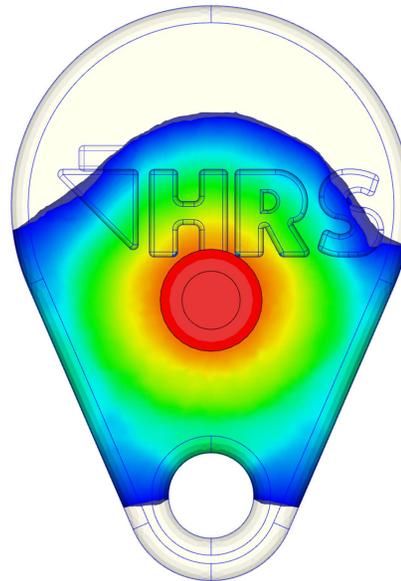
Side A



Side B



BALANCE FILLING



Effect of Optimization: Simulation Results

OPTIMIZED DESIGN

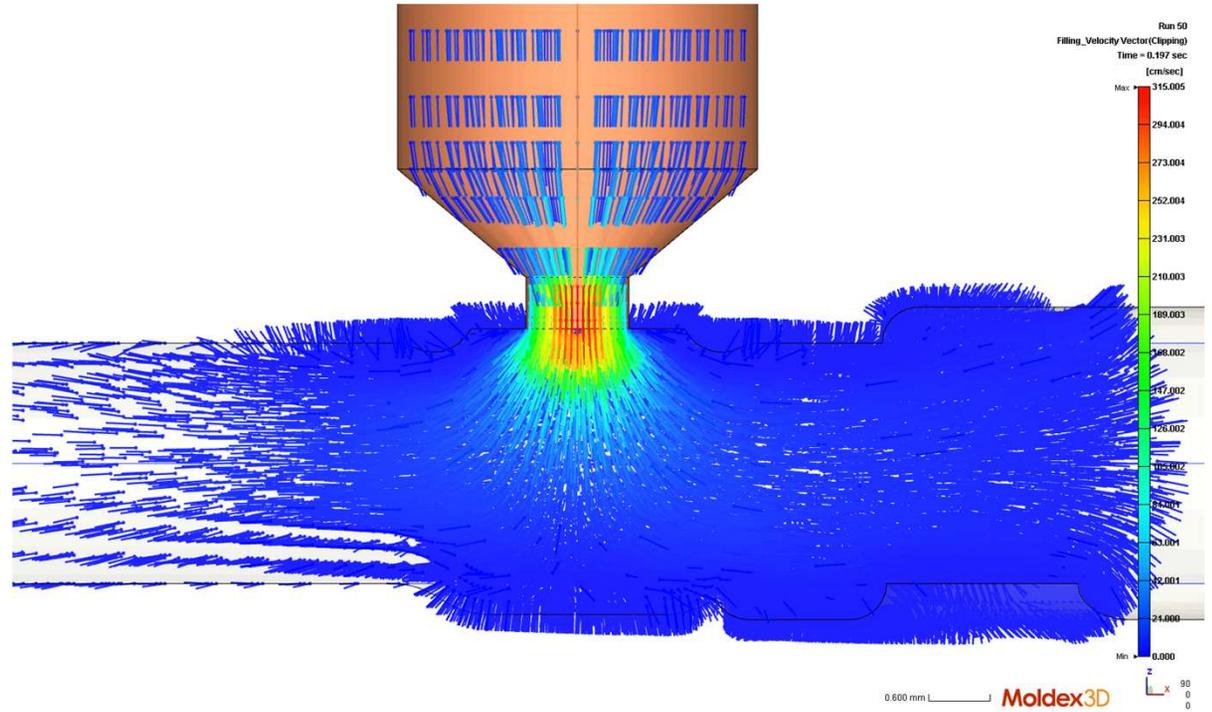
Side A



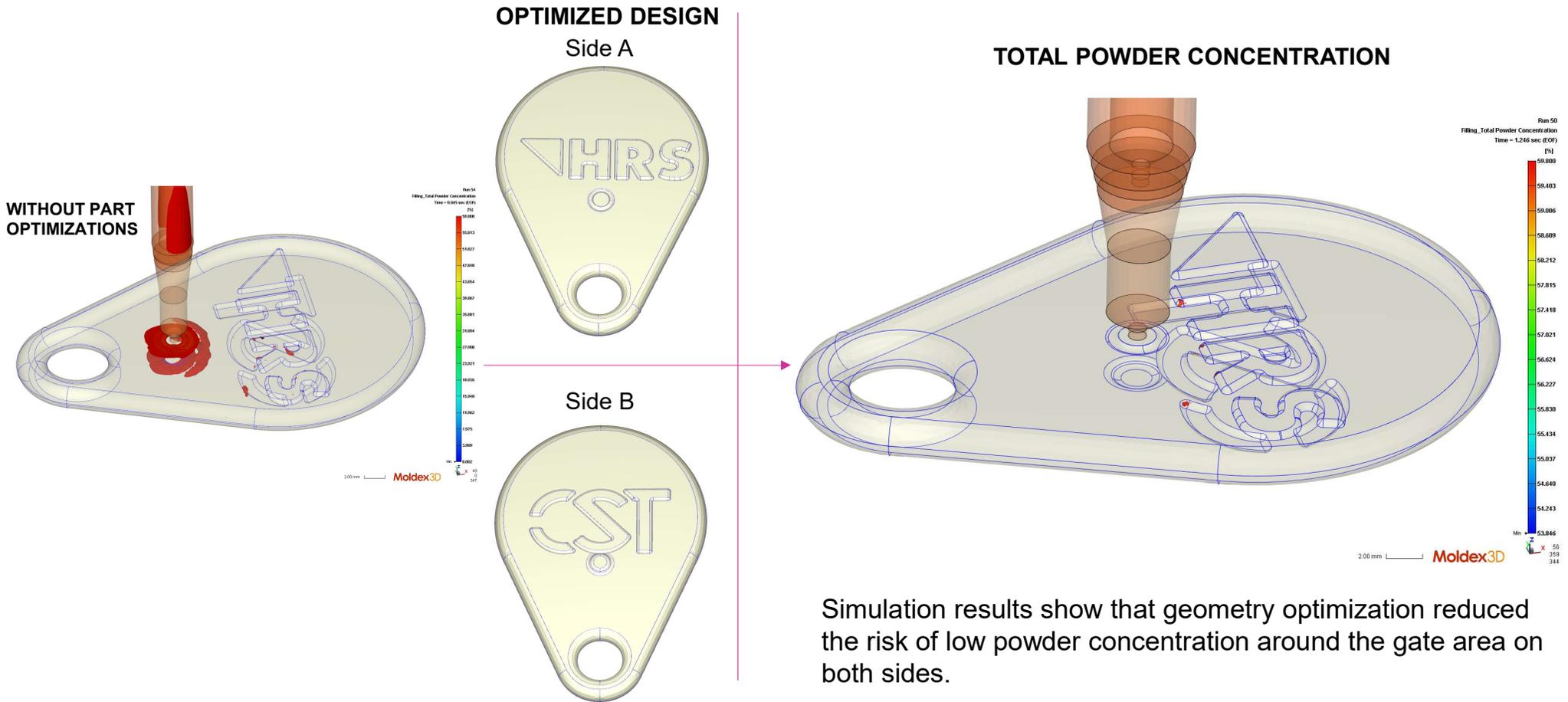
Side B



UNIFORM FLOW FRONT



Effect of Optimization: Simulation Results



From simulation to practice

Side A



OPTIMIZED DESIGN

Side B



GREEN PART: From analysis to implementation, the results confirm that gate design optimization improves the aesthetics of the final part already on the green part.



From simulation to practice

Side A



OPTIMIZED DESIGN

Side B



FINISHED PART: After sintering and polishing, the part maintains good surface aesthetics.



Conclusion

Side A



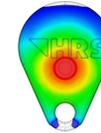
Side B



Direct Injection Tips – MIM

1) Optimized Gate Location

→ Balanced Filling



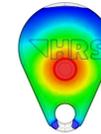
Conclusion



Direct Injection Tips – MIM

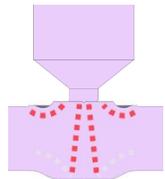
1) **Optimized Gate Location**

→ Balanced Filling



2) **Add a localized thickness increase on both sides**

→ Avoid Halo and Low Powder Concentration



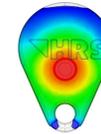
Conclusion



Direct Injection Tips – MIM

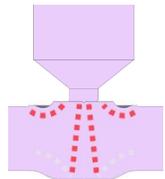
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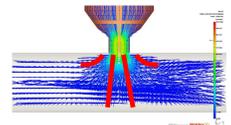
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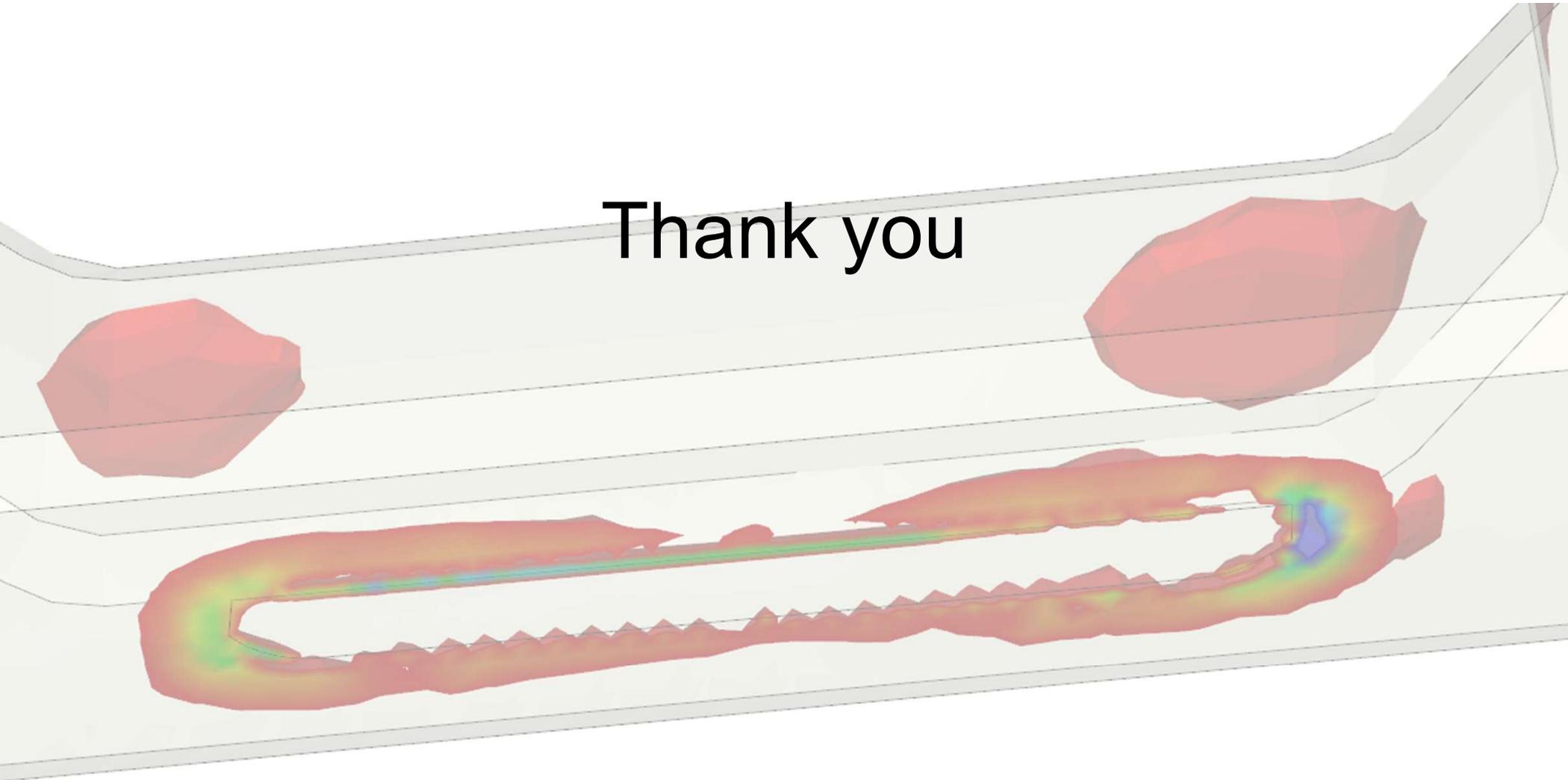
3) **Introduce a circular ring under the gate**

→ Ensure proper material flow



The optimizations are function of gate dimension and thickness of the part.

Thank you



Thank you

